|| |h

I)

$$CF \times h = W \times r$$

$$m (w)^{2}r \times h = m (q \times r)$$

$$w)^{2} h = q$$

$$h^{2} = 1.5^{2} - .5^{2}$$

$$h^{2} = 2$$

$$h^{2} = 1.4142$$

$$w^{2} = \frac{9.81}{12}$$

$$w = 2.6337 \text{ ad}_{5}$$

$$t = 2\pi$$

$$w$$

$$t = 2\pi$$

$$w$$

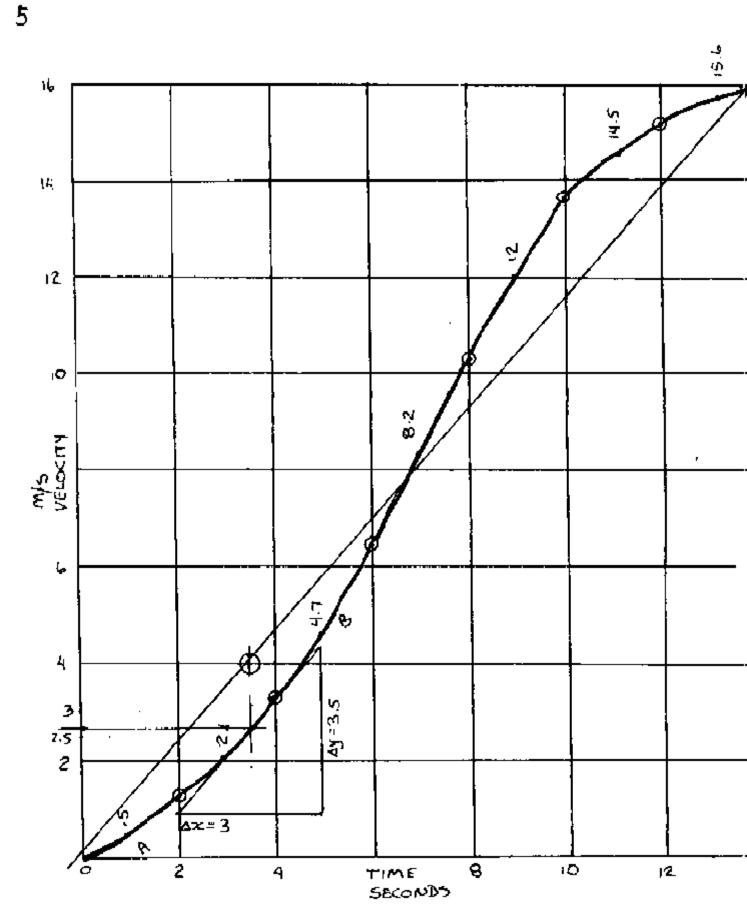
$$t = 2.6337$$

$$M = \frac{1}{26} \times Volume \qquad KE = \frac{1}{2} M V^{2} \\ KE = \frac{1}{2} M V^{2} \\ KE = \frac{1}{2} M V^{2} \\ KE = \frac{1}{2} (140.5) \\ ME = 4140.5 \\ ME = 4140.5 \\ MOLUME = 4140.5 \\ VOLUME = 4140.5 \\ \frac{1}{2} \frac{2}{2} \frac{1}{2} \frac{1}{2}$$

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

4)

Power = T w  
T = F + d  
F = , wN  
F = , o2 Y 50 X 10<sup>3</sup>  
F = 1000  
T = 1000 X d  
d = 
$$\frac{1 + f_2}{2}$$
  
d = ,  $\frac{2 + ... + f_2}{2}$   
d = .1625  
T = 1000 X .1625  
T = 162.5  
Power = 162.5 X w  
 $\omega = 247 \times \frac{120}{60}$   
 $\omega = 12.566$   
Power = 162.5 Y 12.566  
= 2042.03 w  
= 2.04 RW



This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

$$\begin{array}{rcl} \alpha_{(3.5)} &= & \underline{Ay} \\ && \Delta x \\ \alpha &= & \underline{3.5} \\ && 3 \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s^2 \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rcl} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \end{array}$$

$$\begin{array}{rc} 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ \alpha &= & \underline{1.166} \, m/s \\ 1.166 & \forall & 3.5 &= & \underline{4.081} \, m/s \\ \end{array}$$

DISTANCE TRAVELLED = 115.2 m

6)

$$\Theta = 165^{\circ}$$
  
 $G = \frac{165}{24} \times 24^{\circ}$   
 $G = \frac{165}{360} \times 24^{\circ}$   
 $G = 2.87979 \text{ radians}$   
 $G = 300 \times 24^{\circ}$   
 $G = 31.4159$ 

$$\omega_{1} = \omega_{1} + \alpha t$$
  
 $3i.4 = 0 + (\alpha \times 8)$ 
  
 $3i.9 = 8\alpha$ 
  
 $\frac{31.4}{8} = \alpha$ 
  
 $3.925 = \alpha - \alpha a_{15}^{3}$ 

$$\frac{T_{1}}{T_{2}} = e^{it} \frac{T_{1}}{T_{2}} = 2.24 \frac{T_{1}}{T_{2}} = 131.44 \frac{T_{1}}{T_{2}} \frac{T_{2}}{T_{2}} = 131.44 \frac{T_{2}}{T_{2}} = \frac{131.44}{T_{2}} \frac{T_{2}}{T_{2}} \frac{T_{2}}{T_{2}}$$

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

$$T_{c} = \frac{1}{3}$$

$$T_{c} = \frac{5250}{3}$$

$$T_{c} = \frac{5250}{3}$$

$$T_{c} = \frac{1750}{2}$$

$$T_{c} = \frac{1750}{3}$$

$$V^{2} = \frac{1750}{.9}$$

$$V^{2} = \frac{1944.44''}{.9}$$

$$V = \frac{1944.44''}{.9}$$

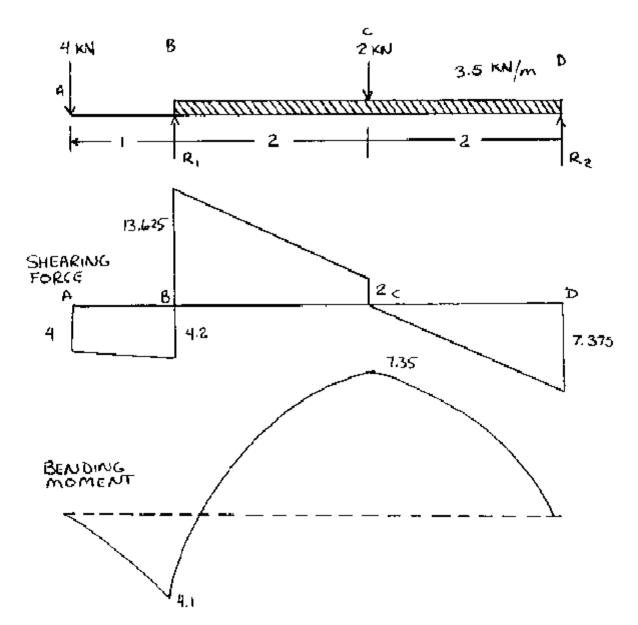
$$V = \frac{1944.44''}{.9}$$

$$V = \frac{1944.09}{.15}$$

$$W = \frac{1940.09}{.15}$$

7) 
$$V = \omega r$$
  
 $V = 2.41 + 1500 \times .15$   
 $v = 23.6 m/s$   
 $m = 1.2 + 10^{3} + 17750 \times 10^{6}$   
 $m = .9 k_{8/m}$   
 $T_{i} = mr^{2}$   
 $T_{i} = .9 + 23.6^{2}$   
 $T_{i} = 502 N$   
 $T_{i} = 502 N$   
 $T_{i} = 502 N$   
 $T_{i} = 502 N$   
 $\frac{100000}{12} = \frac{0.1247005}{12}$   
 $= 4.291$   
 $\frac{11-T_{c}}{12} = e^{-100005/5}$   
 $T_{2} = 76$   
 $\frac{5250 - 502}{12} = 4.291$   
 $T_{2} = 502$   
 $T_{2} = 1610$   
 $f_{0} work = (T_{i} - T_{2}) \times 72$   
 $= 172 \text{ KW}$ 

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net



•

FORCE REQUIRED AT SCRUCE  

$$F = W TAN(B+p)$$
  
 $TAN' G = PITCH
 $TTD$   
 $TAN' G = 25$   
 $TTY 125$   
 $G = 3.64^{\circ}$   
 $F = 308.86 \times TAN(3.64 + 4.57)$   
 $F = 308.86 \times TAN(3.64 + 4.57)$   
 $F = 308.86 \times TAN(3.64 + 4.57)$   
 $F = 44.56 \times 10^{3}$$ 

$$P = T \omega 
\omega = P
T
 $\omega = 31.45 \times 10^{3}$   
 $2785 \times 10^{3}$   
 $\omega = 11.29 \text{ padys}$$$

 $\omega_{i}r_{i}=\omega_{i}r_{\lambda}$ 

$$\begin{aligned}
 f_1 &= 1 \text{ leeth}, & Y_2 &= T \text{ eeth} \\
 \omega_1 T_1 &= \omega_2 T_2 \\
 62.83 &YT_1 &= 11.25 & 80 \\
 T_1 &= 11.25 & 80 \\
 \hline
 T_1 &= 11.25 & 80 \\
 \hline
 G_2.83 \\
 \hline
 T_1 &= 14.375 \\
 \hline
 T_1 &= 14 & T \text{ EETH}
 \end{aligned}$$

A+B = C+D = F+F = G+H = 
$$\int +K = 18072 + \frac{1}{6} = 60$$
  
A+B=60  
A+B=60  
A=  $\frac{K}{J} = \frac{2400}{1600} = \frac{3}{2}$   
B=K  
A=J  
 $3A = 2B$   
 $A = \frac{3}{2}B$   
 $A + B = 60$   
 $\frac{2}{5}B = 60$   
 $\frac{5}{5}B = 60$   
 $\frac{5}{5}A = 60$   
 $\frac{7}{5}A = 60$   

10 cons

$$\frac{F}{E} = r \times \frac{1}{4}$$

$$\frac{F}{E} = -\frac{3}{6} \times \frac{1}{4}$$

$$\frac{F}{E} = -.454$$

$$H = r^{2} + \frac{4}{4}$$

$$H = (-\frac{1}{4}C)^{2} + \frac{4}{4}$$

$$H = -825$$

$$C$$

$$E + F = 6cs$$
 $G + H = 60$ 
 $F = .454E$ 
 $H = .825G$ 
 $E + .454E = 60$ 
 $G + .825G = 60$ 
 $1.454E = 60$ 
 $1.825G = 60$ 
 $E = 60$ 
 $G = 60$ 
 $I.454E = 60$ 
 $I.825G = 60$ 
 $E = 60$ 
 $G = 60$ 
 $I.454E = 60$ 
 $I.825G = 60$ 
 $E = 41.26$ 
 $G = 32.876$ 
 $E = 41.26$ 
 $G = 33.7627H$ 
 $F = 60$ 
 $G = 33.7627H$ 
 $F = 60$ 
 $H = 60$ 
 $F = 60-6$ 
 $H = 60-33$ 
 $F = 19.7627H$ 
 $H = 27.7627H$ 

ļi

BEAM FORCE • 5000 RG × 9.81  
= 49050 N  
= 49.05 RN  
= 49.05 RN  

$$\frac{30KN}{-5--1}$$
  
 $\frac{30KN}{-5--1}$   
 $\frac{30KN}{-5--1}$   
 $\frac{30KN}{-5--1}$   
 $\frac{70KN}{-5--1}$   
 $R_{R}$   
 $R_{R}$ 

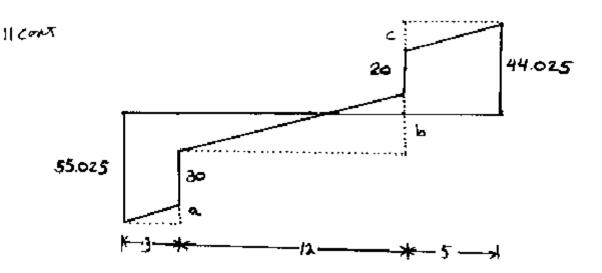
$$30 \times 3 + 49.05 \times 10 + 20 \times 15 = R_{B} \times 20$$
  

$$880.5 = 20 R_{B}$$
  

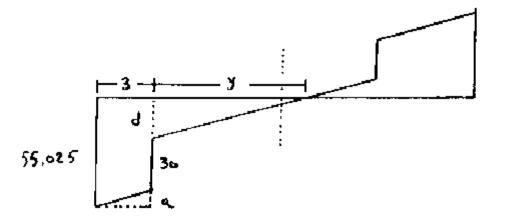
$$R_{B} = \frac{890.5}{20}$$
  

$$R_{B} = 44.025$$

$$R_A + R_B = BEAM FORCE + 30 + 20$$
  
 $R_A = BEAM FORCE - R_B + 50$   
 $R_A = 49.05 - 44.025 + 50$   
 $R_A = 55.025$ 

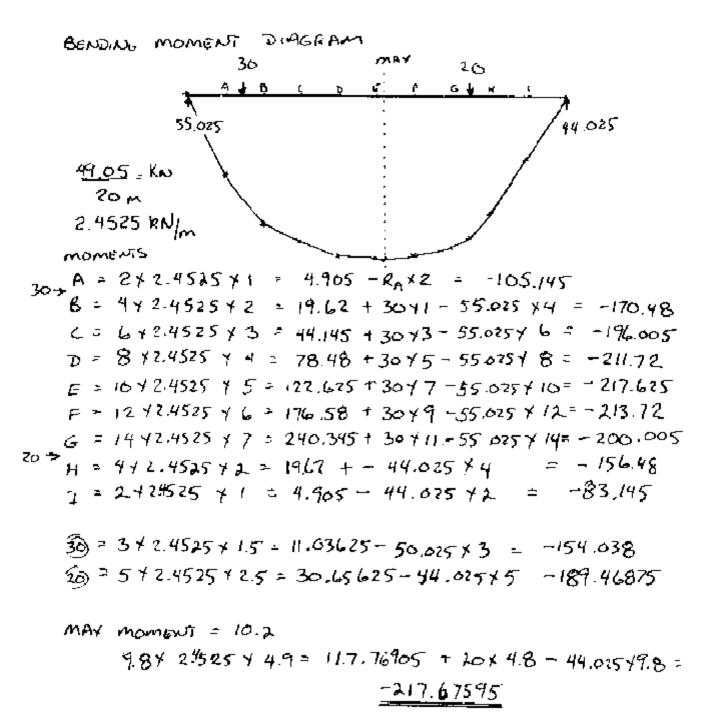


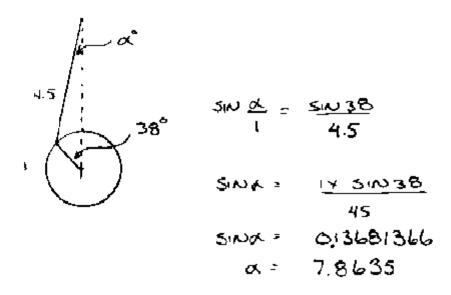
- 4<u>9.05</u>N . 2.4525N
- a = 2.4525 × 3 b=2.4525 × 12 c=24525 × 5 a = 7.3575 b= 29.43 c= 12.2625

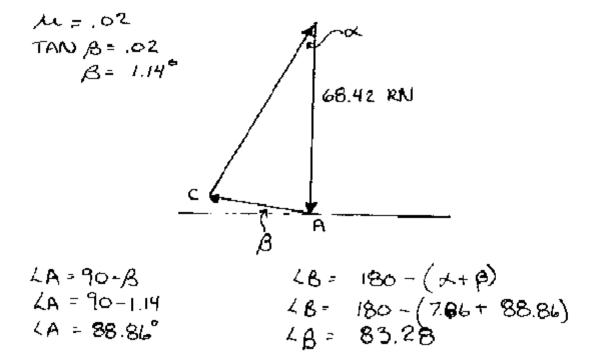


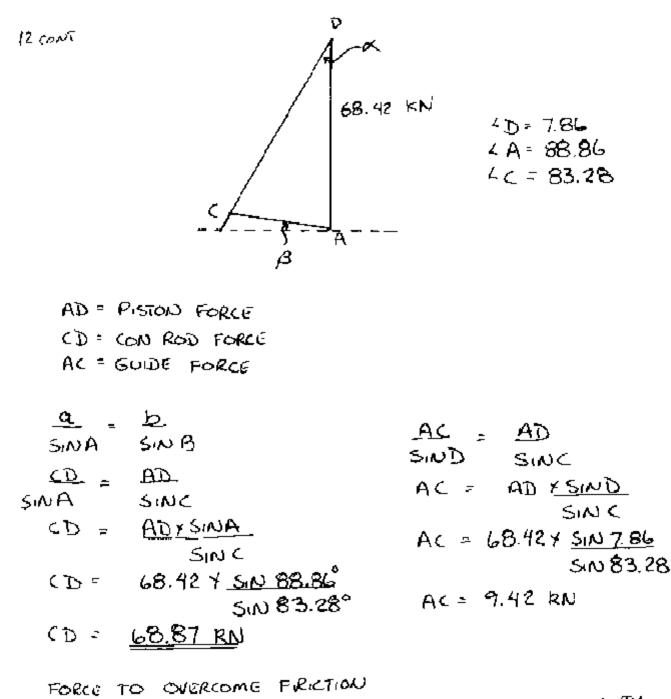
d= 55.025 - a - 30 d= 55.025 - 7.3575 - 30 d= 17.6675N

MAXIMUM MOMENT = 3 + 4 = 10.2 m FROM END CLOSEST TO 30N WEIGHT









CON ROD FORCE WITHOUT FRICTION - CON ROD FORCE WITH F= 68.42 - 68.87 COS 7.86 F= 69.07 - 68.87 F= .19889 RN F= <u>.199 RN</u>

# 14)

$$CF \times h = mg \times \frac{1}{2} TRACK$$

$$\frac{mv^{2}}{r} h = mg \times \frac{1}{2} TRACK \times r$$

$$V^{2} = \frac{mg \times \frac{1}{2} TRACK \times r}{mh}$$

$$V^{2} = \frac{g \times \frac{1}{2} tRACK \times r}{h}$$

$$V^{2} = \frac{9.81 \times .5 \times 2.56 \times 50}{2.45}$$

$$V^{2} = 256.26$$

$$V = 16.01 \text{ M/s} \times \frac{3600}{1000}$$

$$V = \frac{57.63}{k} RM_{hr}$$

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

15)

$$F = m \times \omega \qquad Q = \frac{E}{m}$$

$$a = 9.81 \times \frac{(2.5 - (2.0 \times .02) - 1.5)}{2.5 + 2.0 + 1.5}$$

$$a = \frac{5.886}{6}$$

$$a = 0.981 \text{ m/s}^2$$

$$V^2 = U^2 + 2as$$

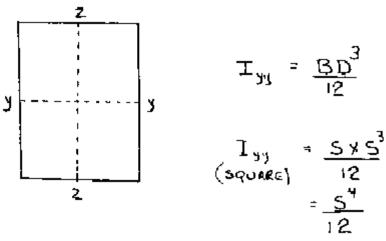
$$V^2 = U^2 + 2x .981 \times 1$$

$$V^2 = 21.981$$

$$V = \frac{1.4}{5} \text{ m/s}$$

PERODIC TIME = 
$$241$$
  
 $\omega$   
 $\omega = \frac{241}{1}$   
 $\omega = \frac{241}{12}$   
 $\omega = \frac{241}{12}$   
 $\omega = \frac{241}{12}$   
 $\omega = \frac{241}{12}$   
 $\omega = \frac{241}{360}$   
 $\omega = \frac{201}{360}$   
 $\Omega = \frac{201}{360}$   
 $\Omega = \frac{201}{360}$   
 $\Omega = \frac{1745}{360}$   
 $\Omega = \frac{1745}{$ 

THE MOMENT OF INERTIA OF A BODY ABOUT ANY AXIS IS EQUAL TO THE MOMENT OF INERTIA OF THE BODY ABOUT A PARALLEL AXIS THROUGH THE CENTRE OF MASS TOGETHER WITH THE PRODUCT OF THE MASS AND THE SQUARE OF THE DISTANCE BETWEEN THE AXIS



POLAR SECOND MOMENT =  $I_p$   $I_p = I_{33} + I_{22}$   $I_p = 5^4 + 5^4$   $I_2 = 12$   $I_p = \frac{25^4}{12}$  $I_p = \frac{5^4}{12}$  18)

$$m_{1} v_{1} + m_{2} v_{2} = m_{1} v_{1} + m_{2} v_{2}$$

$$2 \times 22 + 4 \times 10 = 2 \times v_{1} + 4 \times v_{2}$$

$$84 = 2 v_{1} + 4 v_{2}$$

$$v_{1} = 42 - 2 v_{2}$$

$$v_{1} - v_{2} = -e (v_{1} - v_{2})$$

$$v_{1} - v_{2} = -.08 (22 - 10)$$

$$v_{1} - v_{2} = -9.6$$

$$(42 - 2 v_{2}) - v_{2} = -9.6$$

$$v_{1} = v_{2} - 9.6$$

$$(42 - 2 v_{2}) - v_{2} = -9.6$$

$$v_{1} = 17.2 - 9.6$$

$$v_{1} = -9.6 - 42$$

$$v_{2} = -9.6 - 42$$

$$v_{3} = -9.6 - 42$$

$$v_{4} = -9.6 - 42$$

$$v_{5} = -9.6 - 42$$

$$f = 1$$
  
 $f = 1$   
 $f = 6.0395$ 

PERIODIC TIME = 211 
$$\sqrt{\frac{12}{37}}$$
  
T = 211  $\sqrt{\frac{.064.5}{.064.5}}$   
T = 211  $\sqrt{\frac{.064.5}{.064.5432}}$   
T = 211  $\sqrt{\frac{.064.5432}{.0674.74.01^4}}$   
T = .16558

PERIODIC TIME = 
$$2.6$$
  
 $\omega$   
 $\omega = 2.6$   
 $T$   
 $\omega = 2.6$   
 $\pi$   
 $\omega = 2.6$   
 $16558$   
 $\omega = 37.9465 \text{ rad/s}$   
MAY  $\omega = \omega Y\phi$   
 $= 37.9465 \times 5 \times 2.6$   
 $360$   
 $= 3.31 \text{ rad/s}$ 

$$\begin{array}{r} \mathsf{MAY} \propto = \omega^{2} \phi \\ = 37.9465^{2} \times 5 \times 2.0 \\ 360 \\ = \underline{125.64} \mathrm{rad}/_{3} \end{array}$$

V2

$$\begin{array}{rcl} P_{1} \vee I_{1} - P_{2} \vee V_{2} + \frac{1}{2} m \gamma_{1}^{2} \\ \vee (P_{1} - P_{2}) = \frac{1}{2} m (\gamma_{2}^{2} - \gamma_{1}^{2}) \\ P_{1} - P_{2} = \frac{1}{2} p (\gamma_{2}^{2} - \gamma_{1}^{2}) \\ P_{1} - P_{2} = \frac{1}{2} p (\gamma_{2}^{2} - \gamma_{1}^{2}) \\ P_{1} - P_{2} = \frac{1}{2} p (\gamma_{2}^{2} - \gamma_{1}^{2}) \\ \gamma_{2}^{2} - \gamma_{1}^{2} = 2(P_{1} - P_{2}) \\ \gamma_{2}^{2} - (\cdot 25V_{2})^{2} = 2(\underline{700 - 650}) \\ \cdot 9375 \vee V_{2}^{2} = 100 \quad 1 \\ V_{1}^{2} = 106 \cdot 666^{11} \\ V_{2}^{2} = 106 \cdot 666^{11} \\ V_{1} = \cdot 25V_{2} \\ V_{1} = \cdot 25V_{2} \\ V_{2} = \cdot 20292 \circ 1674 \\ Actual Dischallege = V \times .98 \\ = \cdot 028617641 \end{array}$$

20)

$$P_{1} - P_{2} = \frac{1}{2} \rho \left( V_{2}^{2} - V_{1}^{2} \right)$$

$$U_{1} A_{1} = V_{2} A_{2}$$

$$V_{1} \times .7854 d_{1}^{2} = V_{2} \times .7654 d_{2}^{2}$$

$$V_{2} = V_{1} \times \frac{.7054 d_{1}^{2}}{.7854 d_{2}^{2}}$$

$$V_{2} = V_{1} \times \frac{d_{1}^{2}}{d_{2}^{2}}$$

$$V_{2} = V_{1} \times \frac{d_{1}^{2}}{d_{2}^{2}}$$

$$V_{2} = AV_{1} \times \frac{d_{2}^{2}}{d_{2}^{2}}$$

$$P_{1} - P_{2} = \frac{1}{2} \rho \left( (4V_{2})^{2} - V_{1}^{2} \right)$$

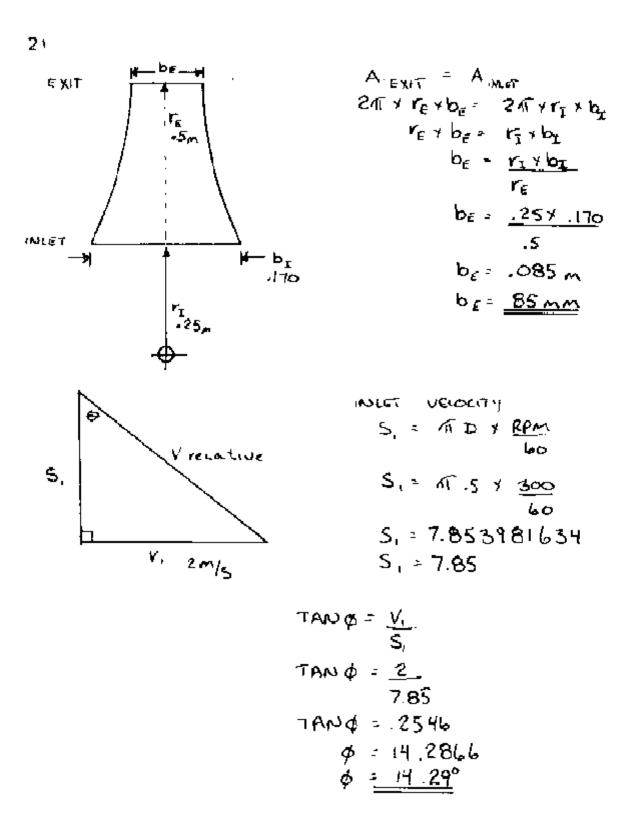
$$P_{1} - P_{2} = \frac{1}{2} \rho \left( 16V_{1}^{2} - V_{1}^{2} \right)$$

$$P_{1} - P_{2} = \frac{1}{2} \rho \left( 15V_{1}^{2} \right)$$

$$I5V_{1}^{2} = \frac{P_{1} - P_{2}}{V_{2}}$$

$$V_{1}^{2} = \frac{P_{1} - P_{2}}{7.5 \rho}$$
(out

CONT



ACCELERATING FORCE = MXQ

$$a = \omega^{2} \times \omega^{2} = \frac{241}{97}$$

$$P_{T} = 1.$$

$$f = \frac{139}{60}$$

$$f = 2.166^{-1}$$

$$P_{T} = .4615$$

$$\omega^{2} = .185.329$$

$$a = .185.329 \times .4$$

$$a = .74.13$$

$$F = .74.13$$

$$F = .74.13$$

$$F = .185.329 \times .4$$

Force By on = hapg  
= .3 × .6×2 ×.8 × 9.81  
= .2.82528 RN  

$$COP_{on} = \frac{2}{3}D$$
  
=  $\frac{2}{3} \times .6$   
 $COP_{on} = .4$   
EQUIVALENT FEAD OF ON = .6 × .8  
1.024  
= .46875 m  
FORCE By WATER = h apg  
=  $(.5 + .46875) \times 14.2 \times 1.024 \times 9.81$   
=  $19.46304$  RN  
 $COP_{WATER} = \frac{2^{NP} nom ENT}{1^{S}} nom ENT}$   
[FROM EQUIV]  
Head  $\frac{1}{2} = \frac{1}{12} \times 1.12 \times (5 + .46875)$   
=  $\frac{2 \times 1^{3}}{12 \times 1.12 \times (5 + .46875)} + (.5 + .46875)$   
=  $\frac{2 \times 1^{3}}{24 \times .96875}$   
=  $1.054771505$   
FROM SURFACE =  $1.055 + [.6 - .46875]$   
=  $1.186021505$ 

23 CONT

$$C \odot P_{wholds} = \frac{1}{3} \times \frac{1}{1} + \frac{1}{1} = \frac{1}{2} \times \frac{1}{3} \times \frac{1}{3} + \frac{1}{3} \times \frac{1}{3} + \frac{1}{3} \times \frac{1}{3}$$

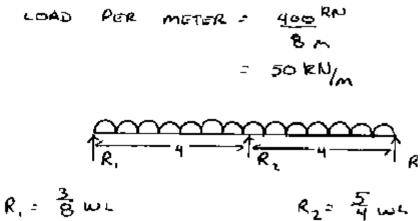
$$I_{o} \omega_{o} = \overline{I_{o}} \omega_{o}$$

$$\omega_{i} = \frac{\overline{I_{o}} \omega_{o}}{\overline{I_{i}}}$$

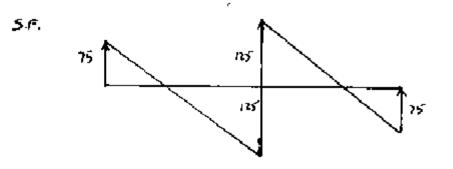
$$\omega_{i} = \frac{4.5 \times 2.1}{1.2}$$

$$\omega_{i} = \frac{23.56 \text{ rad/s}}{1.2}$$

2L



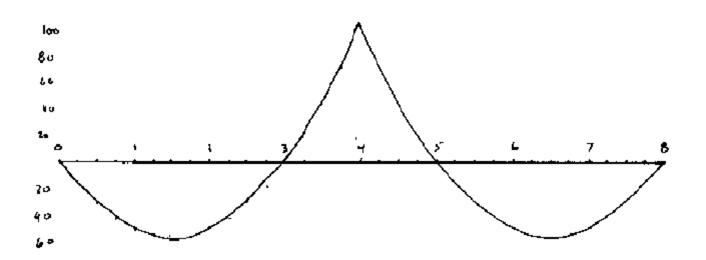




B.M 0  $i (75 \times i) - (1 \times 50 \times .5)$   $i (75 \times i) - (2 \times 50 \times 1)$   $j (75 \times i) - (2 \times 50 \times 1.5)$   $4 (75 \times i) - (4 \times 50 \times 2)$   $5 (75 \times 5) + (250 \times i) - 5 \times 50 \times 2.5$  i = 0 i = -100 i = -1000 i = -1000 i = -1000i = -

#### 26 CONT

BENDING MOMENTS  $\mathbf{O}$  $\mathbf{O}$ - 0 .25 ¥ 75 + .25 ¥50 ¥ .125 .25 = 17,19 5 Y 75 + .5 Y 50 Y .25 - 5 = 31.25 75 + 75 + .75 + 50 × .375 .25 = 42.19 1 1475 + 14504.5 : 50.00 1.25 1.25475 + 1.25450× .625 = 54.69 1.5 1.5+75 + 1.5+50 + .75 = 56.25 1.75 1.75×75 + 1.75×50 × 8.75 = 54.69 2475 + 245041 Ż 2 50 2.25 475 + 2.25 Y 50 X1.125 2.25 ×75 + 2.25 × 50×1.125 = 42.19 2.5 × 75 + 2.5 × 50 × 1.25 = 31.25 2.25 2.5 2.75 ×75 + 2.75 × 50 × 1.375 = 17.19 2.75 3475 + 3450 ×1.5 3  $\geq o$ 3.25 3.25 + 75 + 3.25 + 50 +1.625 = -20.3 3.5 + 75 + 3.5 + 50 + 1.75 = +13. 75 3.5 3.75 + 75 + 3.75 + 50 + 1.875 3.75 = -70.3 4 475 + 44 5042 4 - -100



27  

$$\begin{array}{c}
 & \underbrace{AL} \\
 & \underbrace{C} \\
 & \underbrace{AL} \\
 & \underbrace{C} \\
 &$$

.

$$\vec{C}_{B} = \frac{\vec{E}_{B} \times \vec{O}_{S}}{\vec{E}_{S}}$$
$$\vec{C}_{B} = \frac{90}{200} \times \vec{O}_{S}$$

LOAD CARRIED BY BRASS + STEEL = TOTAL LOAD  
LOAD = 
$$d \neq AREA$$
  
 $d_{B} \neq A_{B} + d_{S} = 37.28 \pm 10^{3}$   
.45 $d_{S} \times .7854 \pm (.04^{2} - .032^{2}) + d_{S} \times .7854 \pm .03^{2} = 37.28 \pm 10^{3}$   
2.0357568  $\pm 10^{-4}d_{S} + 7.0686 \pm 10^{-4}d = 37.28 \pm 10^{3}$   
9.1043568  $\pm 10^{-4}d_{2} = 37.28 \pm 10^{3}$   
 $d_{S} = 40947428.6$   
 $d_{B} = .45 \pm 40.75 \pm 10^{6} N/m^{2}$   
 $d_{B} = .45 \pm 40.75 \pm 10^{6} N/m^{2}$   
 $d_{B} = 28.12 \pm 10^{6} \pm 18.43 \pm 10^{6}$   
 $d_{B} = .46.55 \pm 10^{6} N/m^{2}$ 

$$P_{1} - P_{2} = \rho d h$$

$$P_{1} - P_{2} = (13.6 - .85) \times 9.81 \times .2$$

$$P_{1} - P_{2} = 25.0155 \text{ RN}_{\text{Im}^{2}}$$

$$V_{1} = V_{1} \frac{\alpha_{1}}{\alpha_{2}}$$

$$V_{2} = V_{1} \times \frac{7854 \times .1^{2}}{.7854 \times .03^{2}}$$

$$J_{2} = V_{1} \times 1111$$

$$\frac{P_{1}}{P_{1}} + \frac{V_{1}^{2}}{29} = \frac{P_{2}}{P_{3}} + \frac{V_{2}^{2}}{29}$$

$$\frac{P_{1}}{P} + \frac{V_{1}^{2}}{2} = \frac{P_{2}}{P_{1}} + \frac{V_{2}^{2}}{2}$$

$$\frac{P_{1}}{P} - \frac{P_{2}}{2} = \frac{V_{2}^{2}}{.} - \frac{V_{1}^{2}}{.}$$

$$2(P_{1} - P_{2}) = \mathcal{O}(V_{2}^{2} - V_{1}^{2})$$

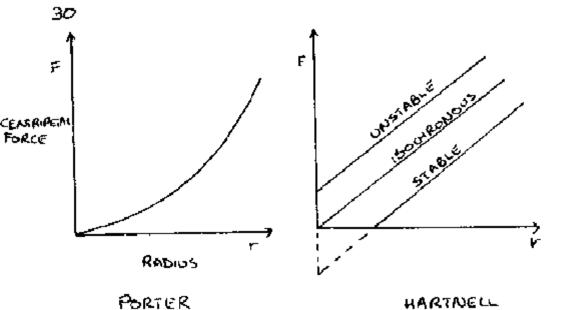
$$\frac{2 \times 25.0155}{.85} = (11.11V_{1})^{2} - V_{1}^{2}$$

$$58.86 = (123.456 - 1)V_{1}^{2}$$

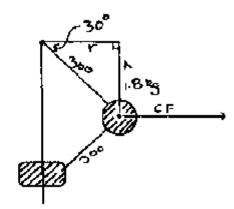
$$.48065934 = V_{1}^{2}$$

VOLUME FLOW = 
$$A, XV_1$$
  
= .7854  $\neq .1^2 \times .6933$   
= 5.4451782  $\neq 10^{-3} m^{3}/s$ 

ACTUAL VOLUME FLOW = VOL FLOW × DISCH COEF  
= 
$$5.44 \times 10^{-3} \times .98$$
  
=  $5.336274636 \times 10^{-3}$ 



PORTER



$$\omega = 120 \times \frac{241}{60}$$

$$\omega = 12.566 \text{ molys}$$

$$h = 300 \cos 30^{\circ}$$

$$h = 300 \times .866$$

$$h = 259.8 \text{ mm}$$

$$h = .259.8 \text{ m}$$

$$h = \frac{q}{\omega^2} \left[ \frac{m+M}{m} \right]$$

$$\frac{h\omega^2}{g} = \frac{m+M}{m}$$

$$\frac{h_{w}}{g} = m + M$$

ŀ

$$\frac{h \omega^{2} m}{g} = m_{1} M$$

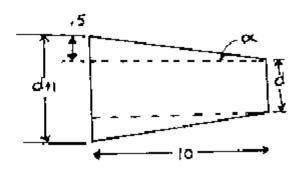
$$\frac{g}{g}$$

$$M = \frac{h \omega^{2} m}{g} - m$$

$$\frac{g}{g}$$

$$M = \frac{.2598 \times 12.566^{2} \times 1.8}{9.81} - 1.8$$

$$\frac{M}{g} = \frac{5.727}{R_{g}} R_{g}$$



ταν α = <u>ο</u> α	TAN $\phi$ = COEFFICIENT OF FRICTION
TANØ = <u>.5</u> 10	TAN & = Ju
TAN & 2,05	TAN $\phi = .18$

FORCE TO DRIVE IN • 2 Y W Y TAN ( $\phi + \alpha$ ) W =  $\frac{F}{2Y(TAN\phi + TAN\alpha)}$ W =  $\frac{500}{2Y(.18 + .05)}$ W = 1086.956 W = 1086.956 W =  $\frac{1086.966}{N}$ FORCE TO DRIVE OUT = 2 Y W Y TAN ( $\phi - \alpha$ ) F = 2 Y 1086.96 Y (.18 - .05) F =  $\frac{282.6}{N}$ 

W = AY AL LOAD D = MEAN DIA.

R= MEAN RADIS

d= dia of con

T= STRESS

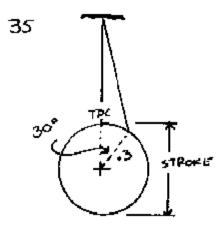
$$T = \prod_{i \in i} d^{3} \prod_{i \in i} T = WR \qquad w=$$

$$R = \frac{WR}{16} \qquad d = \frac{WR}{16} \qquad d = \frac{WR}{16} \qquad d = \frac{WR}{16} \qquad R = .5D$$

$$\Pi = \frac{WR16}{\pi d^{3}} \qquad \Pi = \frac{W.5D16}{\pi d^{3}} \qquad \Pi = \frac{W.5D16}{\pi d^{3}} \qquad \Pi = \frac{WD8}{\pi d^{3}} \qquad \Pi = \frac{100}{\pi d^{3}} \qquad \Pi = \frac{1000}{\pi d^{3}} \qquad \Pi = \frac{100}{\pi d^{3}} \qquad \Pi =$$

VOLUME FLOW = AREA × VELOCITY  
= .7854 × 
$$d^2$$
 × V  
= .7854 × .025<sup>2</sup> × 28  
= .0137445 m/s  
MASS FLOW = VOLUME FLOW × DENSITY  
= .0137445 × 1000  
= .0137445 × 1000  
= .13.7445 × 1000  
= .13.7445 × 1000  
= .0137445 × 1000  
= .0137445 × 1000

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net



This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

## 3•)

$$f = \frac{1}{2\pi} \sqrt{\frac{5}{m}}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{200}{5}}$$

$$f = \frac{1.0066}{5} H_Z$$

$$f = \frac{1.0066}{5\pi} \frac{H_Z}{M}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{5}{3}}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{200}{5 + \frac{75}{3}}}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{200}{5 + \frac{75}{3}}}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{200}{5 \cdot 25}}$$

$$f = \frac{982}{5} H_Z$$

-

37 L SIN 60 L COS L 0.27 ¢ں  $\mathfrak{Dow}\mathcal{N}$ NP+Q=W FOG (G) MOMENTS ABOJT PXLSIN60"+ MPXLOS60" = WX = LCOS60"  $P Y \perp \underline{SIN60} + \mu P \times \underline{LCOS60} = \omega Y \pm \underline{LCOS60} + \mu P \times \underline{LCOS60} + \omega Y \pm \underline{LCOS60} + COS60$  $P \times \underline{SiN60} + \mu P = \pm \omega$ PY TANGO + MP = = = = = = = 2 PTAN 60 + 2MP = W

2PTAN 60° + 2 MP = MP + Q

37 CONT  
LEFT = RIGHT  

$$\mu \varphi = P$$
  
 $Q = \frac{P}{P}$   
 $Q = \frac{P}{P}$   
 $Q = 3.7P$   
2 P TAN 60° + 2 $\mu P = \mu P + \varphi$   
2 P TAN 60° + 2 $\mu P = \mu P + 3.7P$   
2 TAN 60° + 2 $\mu = \mu + 3.7P$   
2 TAN 60° + 2 $\mu = \mu + 3.7$   
 $2\mu = \mu = 3.7 - 2 TAN 60°$   
 $\mu = 3.7 - 2 TAN 60°$   
 $\mu = .2358$ 

M = .24

JL = .15

38 CONT

- = 163.4J
- WORK DONE TO TO STRETCH ROPE = 3747.684.016 = 59.96 J
- WORK DONG AGAINST FRICTION = 163.4-59.96 = 103.44 J

.

$$\begin{aligned} I &= I = G \\ J & r & L \end{aligned}$$

$$\begin{aligned} I &= I \\ T &= I \\ r & r & 2 \\ T &= 2 \times I \\ D \\ T &= (2T) \times J \\ T &= (2T) \times J \\ J &= T \\ 32 \end{aligned} (D^{4} - d^{4}) \\ T &= (2T) \times I \\ D \\ T &= (2T) \times I \\ D \\ 32 \end{aligned}$$

$$\begin{array}{c} (D) & 32 \\ T = & 2 T \Pi & (D^{4} - d^{4}) \\ & 32 D \\ T = & T \Pi & (D^{4} - d^{4}) \\ & 16 D \end{array}$$

39 CONT

$$U = \frac{\pi}{16D} \frac{\pi}{16D} \left( \frac{D^{4} \cdot d^{4}}{DG} \right) \times \frac{2\pi}{DG} \times \frac{1}{2}$$

$$U = \frac{\pi}{16D^{2}G} \frac{\pi}{16D^{2}G} \times (D^{4} \cdot d^{4})$$

$$U = \frac{\pi^{2}\pi}{16D^{2}G} \times (D^{2} - d^{2}) (D^{2} + d^{2})$$

$$U = \frac{\pi^{2}}{46} \left[ \left( \frac{\pi}{4} \right) (D^{2} - d^{2}) L \right] = \frac{D^{2} + d^{2}}{D^{2}}$$

VOLUME OF SHAFT = AREA Y LENGTH  
= 
$$\Pi \times (D^2 - d^2) \times L$$
  
H  
 $U = \left[ \frac{1}{4} \right] \times \left[ \frac{D^2 + d^2}{D^2} \right] \times VOLUME OF SHAFT= \left[ \frac{4}{4} \right] \left[ \frac{D^2}{D^2} \right]$ 

AREA HOLLOW SHAFT = AREA SOLID SHAFT  $\frac{\Lambda\Gamma}{\Pi} \left( D^2 - d^2 \right) = \frac{\Lambda\Gamma}{4} d_s^2$   $\frac{D^2 - d^2}{4} = \frac{d_s^2}{4}$   $\frac{D^2 - d^2}{2} = \frac{d_s^2}{4}$   $\frac{D^2 - d^2}{2} = 22500 \text{ mm}$ 

39 CONT  
STRAIN ENERGY HOLLOW = STRAIN ENERGY SOLID  

$$\frac{T^{2}}{46} \left( \frac{D^{2} + d^{2}}{D^{2}} \right) \neq VOLUME = 1.2 \ Y \frac{T}{46} \neq VOLUME$$

$$\left( \frac{D^{2} + d^{2}}{D^{2}} \right) = 1.2$$

$$D^{2} + d^{2} = 1.2D^{2}$$

$$+ \frac{D^{2} + d^{2} = 1.2D^{2}}{D^{2} + d^{2} = 22500}$$

$$2D^{2} = 1.2D^{2} + 22500$$

$$2D^{2} - 1.2D^{2} = 22500$$

$$D^{2} - d^{2} = 22500$$

$$28125 - d^{2} = 22500$$

$$d^{2} = 28125 - 22500$$

$$d^{2} = 5625$$

$$d^{2} = 5625$$

43)

$$d_{1} = \frac{P \times d}{25}$$

$$d_{1} = \frac{3500 \times 10^{3} \times 1.8}{27.03}$$

$$d_{1} = 105 \times 10^{6} N/m^{2}$$

$$d_{1} = 105 MN/m^{2}$$

$$SEAM d_{min} \frac{d}{2}$$

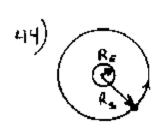
$$= \frac{105}{2}$$

$$d_{2} = \frac{52.5 MN/m^{2}}{2}$$

$$d_{3} = \frac{52.5 MN/m^{2}}{2}$$

$$d_{4} = 34^{6}$$

$$d_{5} = 34^{6}$$



$$R_{E} = 6380$$

$$R_{S} = R_{E} + 650$$

$$R_{S} = 6380 + 650$$

$$R_{S} = 7030$$

$$V = R_{E} \sqrt{\frac{9}{R_{S}}}$$

$$V = 6380 \sqrt{\frac{9.81}{7030}}$$

$$V = 7535.3487 m_{1s}$$

$$V = \underline{D} \qquad t = \underline{D} \\ + \qquad V \\ t = \frac{44170.7927 \times 10^{3}}{7535.3487} \\ + = 5861.8_{5} \\ t = 5861.8_{5} \\ t = 5861.8_{5} \\ 3600 \\ t = 1.628 \\ hours$$

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

45 j

ENERGY ABSORBED BY CABLE = 
$$\Delta KI NETK ENERGY$$
  

$$\frac{\partial^{2} \times V}{2E} = \frac{m V^{2}}{2}$$

$$\frac{\partial^{2} \times V}{2E} = m \sqrt{2}E$$

$$\frac{\partial^{2} = m \sqrt{2}E}{V}$$

$$\frac{\partial^{2} = 2000 \times .6 \times 200 \times 10^{9}}{1200 \times 10^{5} \times 15}$$

$$\frac{\partial^{2} = 8 \times 10^{15}}{1200 \times 10^{5} \times 15}$$

$$\frac{\partial^{2} = 89.44 \times 10^{6} N/m^{2}}{M}$$

$$E = EORCE - AREA - AL$$

$$E = FORCE \times L$$

$$AREA \times \Delta L = FORCE \times L$$

$$\Delta L = FORCE \times L$$

$$AL = FORCE \times L$$

$$AL = FORCE \times L$$

$$AL = S9.44 \times 10^{6} \times 15$$

$$200 \times 10^{7} \times 15$$

$$AL = 6.708 \times 10^{7} \text{ M}$$

$$\Delta L = \frac{6.7 \text{ mm}}{M}$$

46)

$$\omega_{2} = \omega_{1} + \alpha t$$

$$\Delta t = \omega_{2} - \omega_{1}$$

$$\Delta = \frac{\omega_{2} - \omega_{1}}{t}$$

$$\Delta = \frac{2\pi 2000}{60 \times 10} - \frac{2\pi 50}{60 \times 10}$$

$$\alpha = 20.94 - .52$$

$$\alpha = 20.42 \text{ rad/}_{5^{2}}$$

$$T = T\alpha$$

$$T = mR^{2}\alpha$$

$$T = mR^{2}\alpha$$

$$T = 100 \times .8^{2} \times 20.42$$

$$T = 1306.9 \text{ Nm}$$

## 47)

-

$$\beta = 98 MR$$

4Ð

TIME TO STOP ASCENDING  

$$V_2 * V_1 - at$$
  
 $t = V_1 - V_2$   
 $t = V_1 - V_2$   
 $a$   
 $t = 5 - 0$   
 $9.81$   
 $t = .51$  (TIME UP)  
DISTANCE TRAJELLED ASCENDING  
 $S = V_1 + V_2 \times t$   
 $2$   
 $S = 5 + 0 \times .51$   
 $2$   
 $S = 1.275$   
TOTAL DISTANCE TO GROUND = HEIGHT + DISTANCE TRAV  
 $= 420 + 1.275$   
TIME TO DECEND FROM MAYIMUM HEIGHT  
 $S = V_1 t + \frac{1}{2}at^2$   
 $S = 0 + \frac{1}{2}at^2$   
 $t^2 = \frac{2}{2} + \frac{421.275}{9.81}$   
 $t^2 = \frac{2}{2} + \frac{421.275}{9.81}$   
 $t^2 = 9.81$   
 $t^2 = 9.275$  (TIME DOWN)  
TOTAL TIME \* TIME UP + TIME DOWN  
 $= .51 + 9.27$   
 $= 9.785$ 

49  
49  

$$R_1$$
  
 $R_2$   
 $R_1$   
 $R_2$   
 $R_3 = \frac{30}{2}$   
 $R_1 - R_2 = 15^{\circ}$   
 $R_1 - R_2 = 16.82323 \text{ mm}$   
 $R_1 = 16.823 + R_2$   
 $R_2 = 150 \times 2$   
 $R_2 = 150 \times 2$   
 $R_1 = 16.823$   
 $R_2 = 150 \times 2$   
 $R_1 = 16.823 + R_2$   
 $R_1 = 16.823 + R_2$   
 $R_2 = 150 \times 2$   
 $R_1 = 16.823 + R_2$   
 $R_1 = 16.823 + R_2$   
 $R_2 = 141.5885 \text{ mm}$   
 $R_1 = 158.4115 \text{ mm}$ 

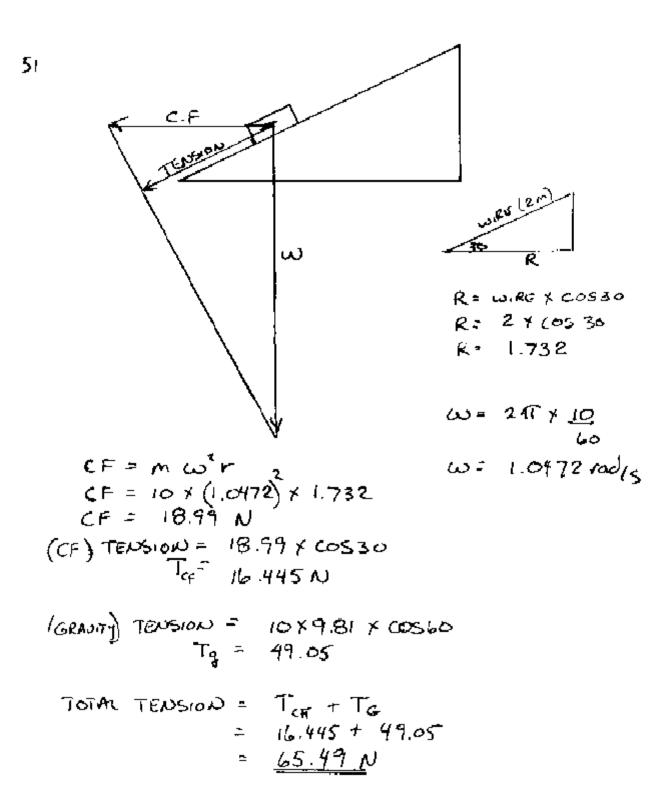
UNIFORM WEAR THEORY

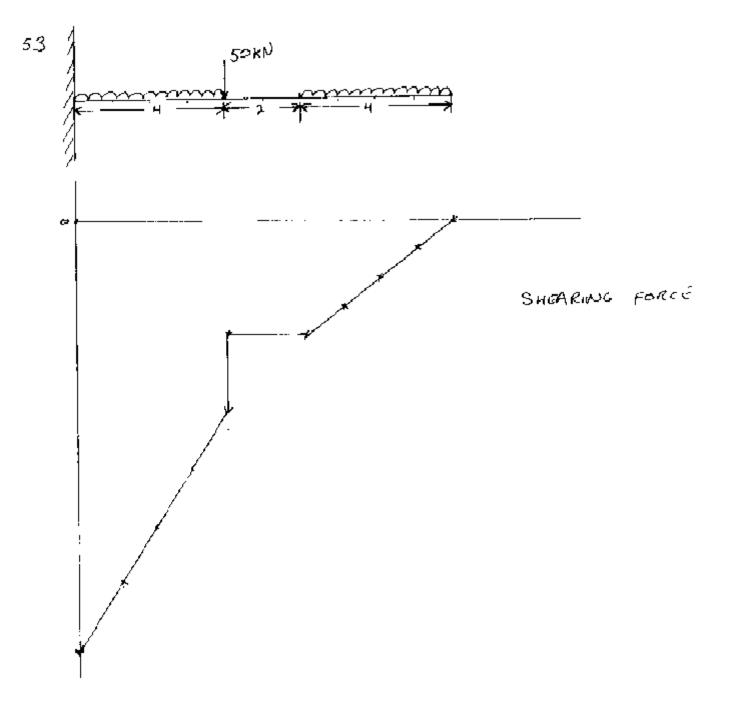
$$T = \underbrace{W R_{m}}_{S_{1} \times i5^{\circ}} \\ W = 2 fi c (R_{1} - R_{2}) \\ c = P \times R_{2} \\ W = 2 fi \times 70 \times i3^{3} \times .1416 \times 16.823 \\ W = 1.0477 \times i0^{6} \\ T = .3 \times 1.0477 \times 10^{6} \times .15 \\ S_{1} \times 15^{\circ} \end{bmatrix}$$

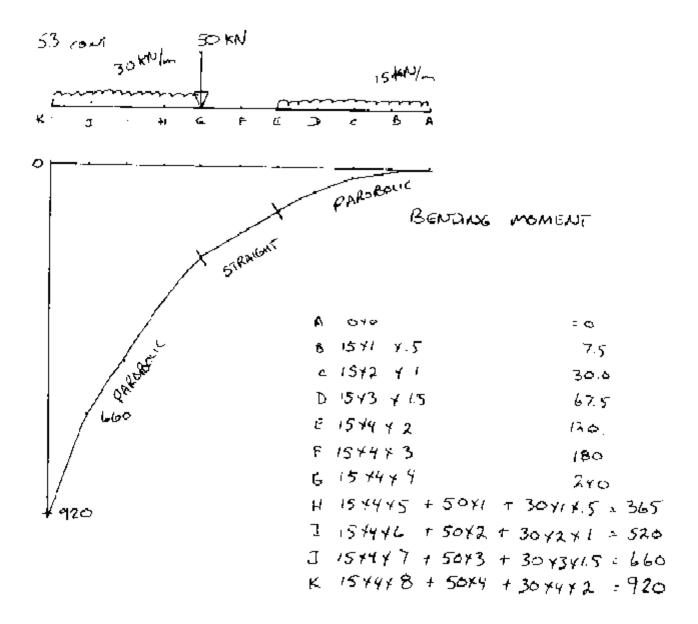
$$T = \frac{.3 \times 1.0477 \times 10^{6} \times 1.5}{\text{SIN 15}^{\circ}}$$
  
T= :82163.3 Nm

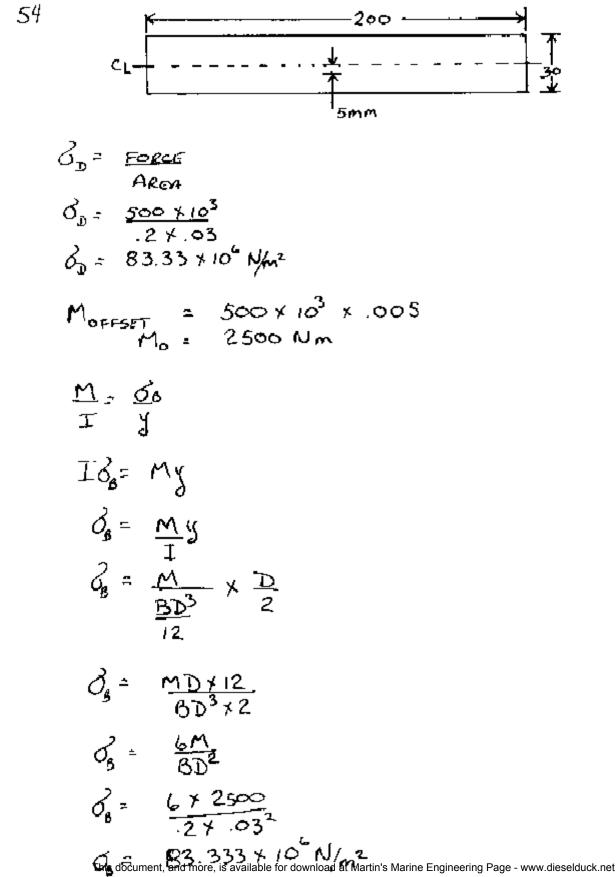
Moments Above privation 
$$P = \frac{1800 \times 400}{9}$$
  
 $P = \frac{1800 \times 400}{300}$   
 $P = \frac{1800 \times 400}{300}$   
 $P = 240 \text{ N}$   
 $R = 240 \text{ Sec 15}^{\circ}$   
 $R = 249 \text{ N}$   
 $R = \cos \varepsilon 45^{\circ} \times T$   
 $T = \frac{R}{COSEC 45^{\circ}}$   
 $T = \frac{176 \text{ N}}{10}$  INITIAL BELT TENSION  
ANGLE OF LAP DRIVING POLLEY = 180 + 30  
 $= 210^{\circ}$   
 $\frac{210}{360} = 3.66 \text{ rad}$   
 $\frac{11}{72} = .3 \times 3.66$   
 $T_1 = 2.71828$   
 $T_2$   
 $T_1 = 176 \times 3$   
 $T_1 = 528 \text{ N}$   
 $POWER = (T_1 - T_2) \vee \text{FD} (T_1 - T_2) \cup V$   
 $P = (518 - 176) \times 247 \times 360 \times .15$   
 $P = \frac{1990 \text{ W}}{100}$ 

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net





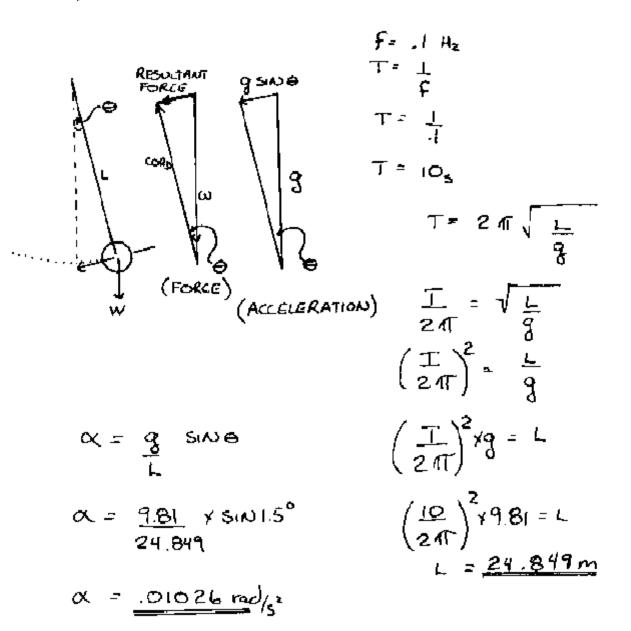




54 com

$$\begin{array}{rcl}
\text{MAYIMUM } \vec{d} &= \vec{d}_{8} + \vec{d}_{9} \\
&= (83.333 + 83.333) \times 10^{6} \\
&= 166.666 \times 10^{6} & N/m^{2} \\
\text{MINIMUM } \vec{d} &= \vec{d}_{9} - \vec{d}_{8} \\
&= (83.333 - 83.333) \times 10^{6} \\
&= \underline{C} & N/m^{2} \\
\end{array}$$





57)  

$$f = \frac{1}{t} \qquad t = 2\pi \sqrt{\frac{1}{9}} \qquad \frac{1}{9.81} \qquad t = \frac{1}{f} \qquad 10 = 2\pi \sqrt{\frac{1}{9.81}} \qquad \frac{10}{9.81} \qquad \frac{10}{2\pi} = \sqrt{\frac{1}{9.81}} \qquad \frac{10}{2\pi} = \sqrt{\frac{1}{9.81}} \qquad \frac{10}{2\pi} = \sqrt{\frac{1}{9.81}} \qquad \frac{5}{4\pi} \qquad \frac{5}{7} \qquad \frac{5}{7} \qquad \frac{7}{9.81} = \frac{1}{8} \qquad \frac{5}{4\pi} \qquad \frac{5}{7} \qquad \frac{5}{7} \qquad \frac{7}{9.81} = \frac{1}{8} \qquad \frac{1}{8} \qquad \frac{5}{4\pi} \qquad \frac{5}{7} \qquad \frac{5}{7} \qquad \frac{1}{9.81} = \frac{1}{8} \qquad \frac{1}{8} \qquad \frac{1}{8} \qquad \frac{5}{8} \qquad \frac{5}$$

$$Q_{=} = g \sin \Theta$$
  
 $Q_{=} = 9.81 \text{ y} \sin 1.5^{\circ}$ 

$$a = .2567 m/s^2$$

-

$$Find the term = Periodic time = 62
20
T = 3.1s
$$I_{0} = m R^{2} = J = 4f D^{1}$$

$$I_{0} = 8 \times .2^{2} = J^{2} = 32$$

$$J = 4f \sqrt{J_{0}} = J^{2}$$

$$I_{0} = .16 \text{ kgm}^{R} = 32 (.004)^{4}$$

$$Periodic time = 24f \sqrt{J_{0}} = J$$

$$\frac{T}{24f} = \sqrt{I_{0}} = J$$

$$\frac{T}{24f} = \sqrt{I_{0}} = \frac{1}{J_{0}} = \frac{1}{J_{0$$$$

**5**,⁼.5

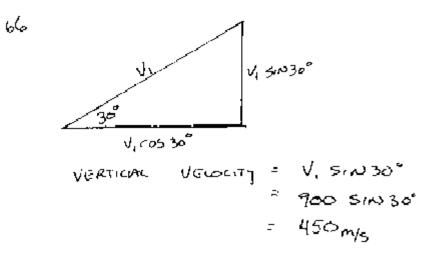
64)

ACCELEDRATING  $S_{A} = \frac{V_{1} + V_{2}t}{2}$   $\frac{2S - V_{1}}{t} = V_{2}$   $\frac{2 \times .5 \sim 0}{-L} = V_{2}$   $\frac{-L}{60}$   $V_{2} = \underline{60 \ \text{km/n}}$ 

DECELERATING

TOTAL DISTANCE TRAVELLES =  $S_A + S_c + S_D$ = .5 + 2 + .75.5 = 2.75 km 65)

TIME TO REACH GROUND  
S. Vit + 
$$\frac{1}{2}at^{2}$$
  
80 =  $\phi$  +  $\frac{1}{2}9.8it^{2}$   
80 = 4.905t^{2}  
 $t^{2} = \frac{86}{4.905}$   
 $t = \frac{4.03855}{5} s$ 



тіме то мах неськт = <u>450</u> 9 ВІ 4 = 45.87 s

MOMENTUM BEFORE - MOMENTUM AFTER  
9.5×10<sup>3</sup> × 18 + 5×10<sup>3</sup>×10.8 = (9.5+5)×10<sup>3</sup> × V  
9.5×18 + 5×10.8 = (9.5+5) V  
171-59 = 14.5V  
177 = 14.5V  

$$V = \frac{117}{14.5}$$
  
 $V = \frac{8.069}{14.5}$  Rm/n IN DIRECTION OF LARGER MISS

$$\frac{3}{2} \times \left(\frac{18 \times 10^{3}}{3600} \times 9.5 \times 10^{3} + \frac{1}{2} 5 \times 10^{3} \times \left(\frac{10.8 \times 10^{3}}{3600}\right)^{2} + \frac{1}{2} 5 \times 10^{3} \times \left(\frac{10.8 \times 10^{3}}{3600}\right)^{2}$$

AFTER IMPACT  

$$\frac{1}{2} \times 9.5 \times 10^{3} \times \left(\frac{8.069 \times 10^{3}}{3600}\right)^{2} + \frac{1}{2} 5 \times 10^{3} \times \left(\frac{8.069 \times 10^{3}}{3600}\right)^{2}$$
  
 $KE = \frac{1}{2} \times \left(\frac{8.069 \times 10^{3}}{3600}\right)^{2} \left(9.5 \times 10^{3} + 5 \times 10^{3}\right)$   
 $KE = 36.422.7$   
 $= 36.4 \text{ KJ}$ 

$$V_{2}^{2} = V_{1}^{2} + 2as$$

$$2as = V_{2}^{2} - V_{1}^{2}$$

$$s = \frac{V_{2}^{2} - V_{1}^{2}}{2a}$$

$$s = \frac{2^{2} - 0^{2}}{2 \times 1 \times 9.81}$$

$$s = \frac{2.0387 m}{2}$$

System EQUIDALENT  

$$\frac{I_{S}}{I_{S}} = \frac{1}{moroR} + \frac{I_{DRUN}}{DRUN} + \frac{1}{cacc} + \frac{1}{1} = eacc + \frac{1}$$

----

$$T = \mu \omega r^{2} \left( \frac{\cos \omega_{1} - \cos \omega_{2}}{\sin \omega_{m}} \right) \left( \frac{\rho_{m} + \rho_{m}'}{\rho_{m}} \right)$$

$$\Theta_{1} = 10^{9}$$

$$\Theta_{2} = 130^{9}$$

$$\Theta_{m} = 90^{9} \text{ if } \Theta_{2} \text{ GREATER THAN 90^{9}}$$

$$\Theta_{m} = \Theta_{2} \text{ if } \Theta_{2} \text{ LESS THAN 90^{9}}$$

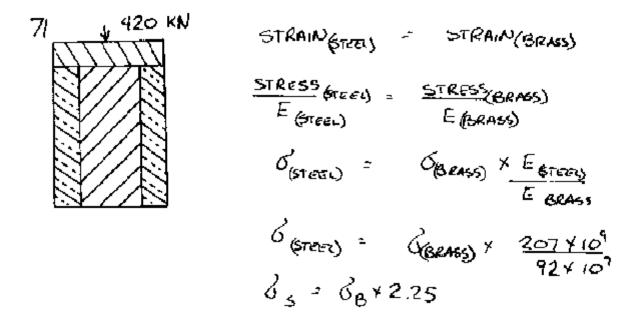
$$T = \mu \omega r^{2} \left[ \frac{\cos 10^{9} - \cos 130^{9}}{\sin 90^{9}} \right] \times (1520 + 480)$$

$$T = .3 \times .05 \times .15^{2} \times \left[ \frac{.984 - (-.642)}{1} \right] \times 2000$$

$$T = 3.375 \times 10^{-9} \times 1.6276 \times 2000$$

$$T = 1.09863 \text{ KNm}$$

.



TOTAL LOAD: LOAD (GREEL) + LOAD (BRASS)  
4120 × 10<sup>3</sup> = 
$$(d_{5} \times A_{5}) + (d_{8} \times A_{8})$$
  
420 × 10<sup>3</sup> =  $(d_{5} \times 2580 \times 10^{-1}) + (d_{8} \times 3225 \times 10^{-1})$   
420 × 10<sup>3</sup> =  $(2.25d_{8} \times 2580 \times 10^{-6}) + (d_{8} \times 3225 \times 10^{-1})$   
420 × 10<sup>3</sup> =  $5.805 \times 10^{-3}d_{8} + 3.225 \times 10^{-3}d_{8}$   
420 × 10<sup>3</sup> =  $9.03 \times 10^{-3}d_{8}$   
46511627.9 =  $d_{8}$   $d_{8} = \frac{46.51}{10} \frac{MN}{m^{2}}$   
 $d_{5} = d_{6} \times 2.25^{-1}$   
 $d_{5} = 46.51 \times 2.25$   
 $d_{5} = 104651162.8$   $d_{5} = 104.65 \frac{MN}{m^{2}}$ 

72  

$$AREA_{(BRASS)} = .7854 \times (D^{2} - d^{2})$$
  
 $= .7854 \times (40^{3} - 32^{2})$   
 $= 452.39 \text{ mm}^{2}$   
 $AREA_{(STEEL)} = .7854 \times D^{2}$   
 $= .7854 \times 30^{2}$   
 $= .7854 \times 30^{2}$   
 $= .7854 \times 30^{2}$ 

FORCE TO COMPLESS BRASS TUBE TO STEEL LENGTH

$$F_{g} = \frac{A E \Delta L}{L}$$

$$F_{0} = \frac{452.39 \times 10^{-6} \times 90 \times 10^{9} \times .125 \times 10^{-3}}{400, 125 \times 10^{-3}}$$

$$F_{g} = 12719.49391 \text{ N}$$

$$F_{g} = 12.72 \text{ kN}$$
FORCE RESISTED BY STEEL BAR = 50 - F\_{g}
$$F_{R} = 50 - 12.72$$

$$= 37.28 \text{ kN}$$

$$E = \frac{FORGE}{AREA}$$

$$\frac{AL}{L}$$

$$\frac{\Delta L}{L} \times E = \frac{fORCE}{AREA}$$

AL = FORCE X L AREA X E

 $\Delta L_{B} = \Delta L_{S}$ 

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

72 const

$$\Delta L = \frac{F_{CRCC} + L}{AROA \times E}$$

$$\Delta L_{B} = \frac{F_{R} \times L}{A_{B} \times E_{B}}$$

$$\Delta L_{S} = \frac{F_{S} \times L}{A_{S} \times E_{S}}$$

$$\frac{F_{R} \times L}{A_{R} \times E_{R}} = \frac{F_{S} \times L}{A_{S} \times E_{S}}$$

$$\frac{F_{R} \times E_{R}}{F_{R}} = \frac{F_{S} \times L}{A_{S} \times E_{S}}$$

$$\frac{F_{R}}{F_{R}} = \frac{F_{S} \times L}{A_{S} \times E_{S}}$$

$$L$$

$$F_{R} = \frac{F_{S} \times A_{R} \times E_{R}}{A_{S} \times E_{S}}$$

TOTAL FORCE =  $F_{B_a} + F_s$  $F_T = \left[ \frac{F_s \times A_B \times E_B}{A_s \times E_s} \right] + F_s$   $F_T = \left[ \frac{A_B \times E_B}{A_s \times E_s} + 1 \right] \times F_s$   $F_s = \frac{F_r}{\left[ \frac{A_B \times E_B}{A_s \times E_s} \right]}$   $F_s = \frac{37280}{(452.39 \times 10^{-6}) \times (90 \times 10^{-1})}$   $(706.86 \times 10^{-6}) \times (700 \times 10^{-1})$ 

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

72 CONT

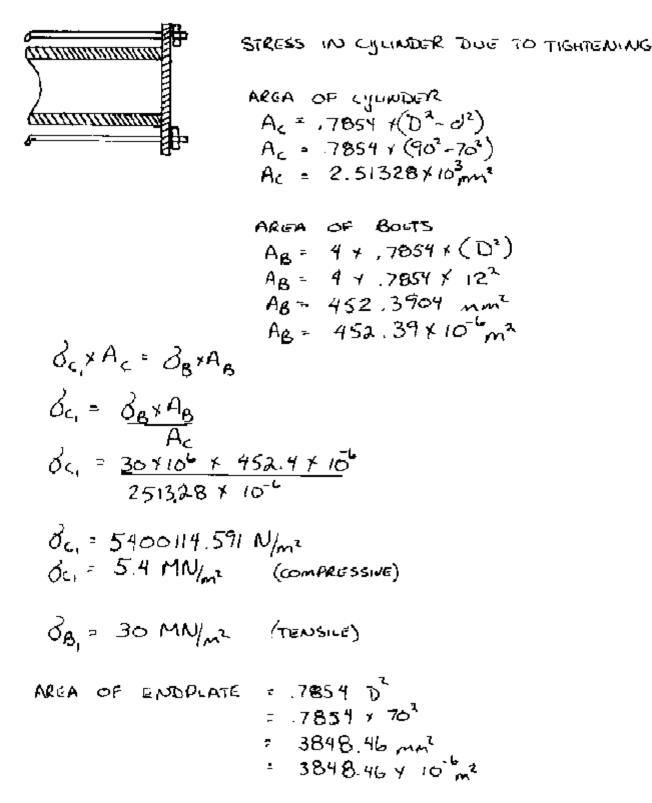
$$F_{B_1} = F_1 - F_5$$
  
 $F_{B_2} = 37.28 - 28.944$   
 $F_{B_1} = 8.336$  RN

$$G_{B} = \frac{LOAD}{AREA}$$
  
 $G_{B} = \frac{21.056 \times 10^{3}}{452.39 \times 10^{56}}$   
 $G_{B} = \frac{46.543911}{46.544} \frac{N/m^{2}}{m^{2}}$ 

$$\delta_{s} = \frac{LOAD}{ARGA}$$

$$\delta_{s} = \frac{28.944 \times 10^{3}}{706.86 \times 10^{-6}}$$

$$\delta_{s} = 40947288$$



## 73.00

$$\mathcal{C}_{B} = \mathcal{C}_{A_{c}} + \mathcal{P}_{c} A_{c}
 \mathcal{C}_{B} = \mathcal{C}_{c} A_{c} + \mathcal{P}_{c} A_{c}
 \mathcal{C}_{B} = \mathcal{O}_{c} A_{c} + \mathcal{P}_{c} A_{c}
 \mathcal{C}_{B} = \mathcal{O}_{c} A_{c} + \mathcal{P}_{c} A_{c}
 \mathcal{C}_{B} = (\mathcal{O}_{c} A_{c} + \mathcal{P}_{c} A_{c}
 \mathcal{A}_{B}
 \mathcal{C}_{B} = (\mathcal{O}_{c} X 2513.3 \times 10^{6}) + (3 \times 10^{6} \times 3849 \times 10^{6})
 452.4 \times 10^{6}
 \mathcal{C}_{B} = 5.555 \mathcal{O}_{c} + 25.524 \times 10^{6}$$

DL IS COMMON TO BUITS AND CYUNDER

ΔL CYLINDER = COMPRESSION BY BOUTS - EXPANSION BY PRUSS ΔLC = ΔLCC - ΔLCC ΔL BOLTS = RESULTANT BY PRESSURE - INITIAL<sup>BY</sup>TENSION ΔLB = 4LBP - ΔLBT

$$\Delta L_{c} = \Delta L_{B}$$

$$\Delta L_{cc} = \Delta L_{BP} = \Delta L_{BT}$$

$$\Delta L_{cc} = \Delta L_{ce} = \Delta L_{BP} = \Delta L_{BT}$$

$$\frac{\partial_{cc} L_{c}}{E} = \frac{\partial_{ce} L_{e}}{E} = \frac{\partial_{BT} L_{B}}{E}$$

$$\frac{\partial_{cc} L_{c}}{E} = \frac{\partial_{ce} L_{c}}{E} = \frac{\partial_{BP} L_{B}}{E} = \frac{\partial_{BT} L_{B}}{E}$$

$$L_{c} \left( \frac{\partial_{cc} - \partial_{ce}}{\partial_{ce}} \right) = L_{B} \left( \frac{\partial_{BP} - \partial_{BT}}{\partial_{BT}} \right)$$

$$L_{B} = 1.1 L_{c}$$

$$L_{c} \left( \frac{\partial_{cc} - \partial_{ce}}{\partial_{ce}} \right) = \frac{1.1 L_{c}}{E} \left( \frac{\partial_{cc} - \partial_{ce}}{\partial_{ce}} \right) = \frac{1.1 L_{c}}{E}$$

$$\begin{aligned} -c \left( \delta_{cc} - \delta_{ce} \right) &= 1.1 \ L_{c} \left( \delta_{BP} - \delta_{BT} \right) \\ \delta_{cc} - \delta_{ce} &= 1.1 \left( \delta_{BP} - \delta_{BT} \right) \\ 5.4410^{4} - \delta_{ce} &= 1.4 \left( \delta_{BP} - 30410^{4} \right) \\ \delta_{ce} &= 5.4410^{6} - 1.1 \left( \delta_{BP} - 30410^{6} \right) \\ \delta_{ce} &= 5.4410^{6} + 33410^{6} - 1.16P \\ \delta_{ce} &= 38.4410^{6} - 1.16P \end{aligned}$$

This document, and more, is available for download at Martin's Marine Engineering Page - www.dieselduck.net

74 cont  
"MINUMUM STRESS = 0"  

$$d_{D} - d_{S} = 0$$
  
 $d_{B} = \partial_{D}$   
 $OB = 22.63 MN/m^{2}$   
 $M = Id$   
 $400 \times 10^{3} \times S = II (D^{4} - d^{4}) \times 22.63 \times 10^{6}$   
 $S = AT + 25^{4} - 2^{4} \times 22.63 \times 10^{6} \times 2$   
 $S = AT + 25^{4} - 2^{4} \times 22.63 \times 10^{6} \times 2$   
 $S = .05124 m$   
 $S = 51.24 mm$ 

Direct compressive stress = 
$$LOAD$$
  
Area  
 $d_{i}^{2} = \frac{500 \times 10^{3}}{.7854(.3^{2} - .25^{3})}$   
 $d_{i}^{2} = 23.148 \mod N_{im^{2}}$   
 $d_{i}^{2} = 23.15 MN_{im^{2}}$   
 $d_{i}^{2} = 23.15 MN_{im^{2}}$   
 $d_{i}^{2} = \frac{M_{i}}{1}$   
 $d_{i}^{2}$ 

75 cont

$$MAYIMUM EYEENTRIK LOADING G - G_B = 0
G_C = 0B
G_B = 23.15 MN/m2
$$M = IG
J
500 Y 103 X S = II × (34-.254) × 23.15 × 106
3
500 Y 103 Y S = II × (34-.254) × 23.15 × 106 × 2
G4 Y .3
S = II × (34-.254) × 23.15 × 106 × 2
500 × 103 × 64 × .3
S = .063542 m
S = .063542 m$$$$

FORCE TO SHEAR COTTER SHEAR STRENGTH & COTTER AREA & SHEAR FACTOR FL = 340 × 10<sup>6</sup> × 6T × 1T × 1.8

$$F_{z} = F_{s}$$

$$340 \times 10^{6} \times 67 \times T \times 1.8 = 460 \times 10^{6} \times (7854 \times .15^{2} - .15 \times 7)$$

$$3672 \times 10^{6} T^{2} = 8.1289 \times 10^{6} - 69 \times 10^{6} T$$

$$3672 T^{2} = 8.1289 - 69 T$$

$$53.22 T^{2} + T = .1178 = 0$$

$$a = 53.22$$

$$b = 1$$

$$T = -b \pm \sqrt{b^{2} - 4ac}$$

$$c = -.1178$$

$$T = -1 \pm \sqrt{1^{2} - 4 \times 53.22 \times (-.1178)}$$

$$2 \times 53.22$$

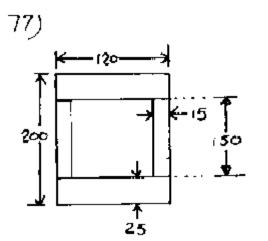
$$T = -1 \pm \sqrt{1 - (-25.077)}$$

$$106.44$$

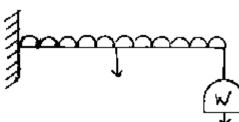
$$T = -1 \pm 5.1065$$

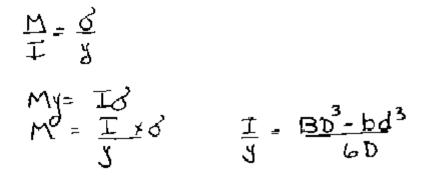
 $T = \frac{4.1065}{106.44}$ T = .03858 m 76 cont

FORCE ON STAY = FORCE ON COTTER  
460 × 10<sup>6</sup> × .7854 × d<sup>2</sup> = 340 × 10<sup>6</sup> × 38.58×231.48 × 1.8  
361.284 × 10<sup>6</sup> d<sup>2</sup> = 5.465 × 10<sup>12</sup>  
d<sup>2</sup> = 
$$5.465 \times 10^{12}$$
  
361.284 × 10<sup>6</sup>  
d<sup>2</sup> = 15.12789  
d = 122.99  
d = 123 mm



VOLUME = 
$$(.2 \times .12) - (.15 \times .09) \times 3$$
  
 $V = .0315 m^3$   
mASS =  $p \neq V$   
=  $7.86 \times .0315$   
=  $247.59 kg$   
FORCE = ma  
=  $247.59 \times 9.81$   
=  $2428.8 N$   
=  $2.429 kN$ 





 $2.429 \neq 1.5 + W \neq 3 = (12 \neq .2^{3}) - (.09 \neq .15^{3}) \neq 45000$   $6 \neq .2$  3.6435 + 3W = 24609375 3W = 24.6094 - 3.6435 3W = 20.965875 W = 20.965875  $W = \frac{6.988}{9.81} \text{ kN} \neq 10^{3}$   $W = \frac{712.4}{9.81} \text{ kg}$ 

- -

$$I = \prod_{r} G G G$$

$$J = \prod_{r} L$$

$$G = \prod_{r}$$

83 cont

SHAFT 
$$T_{s} = \frac{\pi}{J}$$

$$T_{r} = \pi J$$

$$T_{s} = \frac{\pi}{J}$$

FOR LINER 
$$J = \frac{\pi}{32} (D^{4} - d^{4})$$
  
 $T = \frac{\pi}{7}$   
 $T = \frac{\pi}{7} (D^{4} - d^{6}) \pi$   
 $T = \frac{\pi}{32} (D^{4} - d^{6}) \pi$   
 $T = \pi \frac{\pi}{16} \frac{f(29^{4} - 24^{4}) f(1)}{16 f(29^{4} - 24^{4}) f(1)}$   
 $T = .002543 \pi$ 

BBCONT

$$\frac{100 \times 10^{3}}{100 \times 10^{3}} = 002714 \int_{L}^{2} + 002543 \int_{L}^{2} \int_{3}^{2} = 1.773 \int_{L}^{2}$$

$$\frac{100 \times 10^{3}}{100 \times 10^{3}} = 100 \times 10^{3}$$

$$\frac{100 \times 10^{3}}{100 \times 10^{3}} = 100 \times 10^{3}$$

$$\frac{100 \times 10^{3}}{100 \times 10^{3}} = 100 \times 10^{3}$$

$$\begin{aligned}
 \pi_{5} &= 1.773 \, \mathcal{T}_{L} \\
 \vec{T}_{5} &= 1.773 \, \mathcal{T}_{13} \, .59 \, \mathcal{T}_{10}^{b} \\
 \vec{T}_{5} &= \frac{24 \, .11 \, \, \mathcal{K} \, 10^{6} \, \, N/m^{2} \\
 \end{array}
 \end{aligned}$$

$$\Theta = \frac{114}{5} = \frac{124.11 \times 10^{6} \times 4}{.12 \times 90 \times 10^{9}} \times \frac{360}{24}$$

$$\frac{1}{2} gv^{2} = pgh_{h}$$

$$v^{2} = \frac{pgh_{h}}{5} \frac{pgh_{h}}{5}$$

$$v^{2} = \frac{1 \times 9.81 \times .2}{.5 \times 1.3 \times 10^{-3}}$$

$$v^{2} = 3018.46$$

$$v = \frac{54.94}{5} \frac{94}{5} \frac{m/5}{5}$$

•

86)

87  

$$V_{w} = \frac{-s_{2}}{V_{v}}$$
 $V_{1} = \frac{2.4 m/s}{V_{1}}$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) + TAN(180 - 150) = V,$ 
 $(s_{2} - V_{w}) = 4.157 m/s$ 

$$S_{1} = M D N$$

$$S_{2} = M V .355 \times 1000$$

$$S_{2} = 18.5877 m/s$$

$$V_{w} = S_{1} - (S_{2} - V_{w})$$

$$V_{w} = 19.5877 - 4.157$$

$$V_{w} = 14.43 m/s$$

$$H_{T} = \frac{V_{w}}{9} S_{1}$$

$$H_{T} = \frac{14.43 \times 18.5877}{9.81}$$

$$G = .7936$$

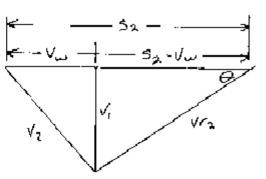
$$H_{T} = 27.3415 m$$

$$G = \frac{79.367}{9}$$

TANO = V.

 $S_2 - V_{\omega} = \frac{V_1}{1ANG}$   $S_2 - V_{\omega} = \frac{1.000}{TAN45}$ 

52-Vw = 2.004



Sy CARCOMFERENCEY Fed Sec S2= AT 4.454 500 S2= 11.781m/s  $V_{\omega} = S_2 - (S_2 - V_{\omega})$ Vw = 11.781 - 2.004 Vw= 9.777 m/s

$$H_{T} = \frac{V_{w}S_{2}}{9}$$

$$H_{T} = \frac{9}{1.777 \times 11.78!}$$

$$H_{T} = \frac{11.74}{9.81}$$

$$V = C_V \times V$$
  
= .97 ×  $\sqrt{2gh}$   
= .97 ×  $\sqrt{2.39.81} \times 10$   
= 13.587 m/s

$$A = C_A + A$$

$$= .64 + .7854 + 20^{2}$$

$$= 201 mm^{2}$$

$$V = A \neq V$$
  
= 201×10<sup>6</sup>× 13.587 × 3600  
= 9.33 m<sup>3</sup>/<sub>h</sub>

.

LOSS of PROSSURG = GAININKE  

$$P_{1}V - P_{2}V = \pm m V_{2}^{2} - \pm n V_{1}^{2}$$
  
 $V(P_{1},P_{2}) = \pm m (V_{2}^{2} - V_{1}^{2})$   
 $P_{1}-P_{2} = \pm m (V_{2}^{2} - V_{1}^{2})$   
 $V$   
 $P_{1}-P_{2} = \pm p (V_{2}^{2} - V_{1}^{2})$ 

$$A_{1}v_{1} = A_{2}v_{2}$$

$$V_{2} = \frac{A_{1}v_{1}}{A_{2}}$$

$$V_{2} = \frac{7854 \times .15^{2}}{.7854 \times .05^{2}} \times V_{1}$$

$$V_{2} = 9 V_{1}^{2}$$

$$P_{1} \cdot P_{2} = 50 \times 10^{3} \times (13.6-1) \times 10^{3} \times 9.81$$

$$P_{1} - P_{2} = 6180.3$$

$$6180.3 = \frac{1}{2} p \left[ (9v)^{2} - v_{1}^{2} \right]$$

$$6180.3 = \frac{1000}{2} \left( 80_{1}^{2} \right)$$

$$6180.3 = 40000 V_{1}^{2}$$

$$1545 = V_{1}^{2}$$

$$393'_{M_{5}} = V_{1}$$

$$f_{cturk} = \hat{m} + c.$$

$$= 25.00 + 10^{3} + .9$$

$$\hat{m} = 22.51 \times 10^{3} \frac{R_{g}}{h_{r}}$$

$$m = 22.51 \times 10^{3} \frac{R_{g}}{h_{r}}$$